

SUPPLEMENT 1

Supplement 1: Rank data of accuracy and precision for different regression equations (or sets of equations), with DXA-determined body fat adopted as reference. If required, the appropriate conversion factors were used for standardisation of the originally published equations. A – females, B – males. p values obtained with one-way ANOVA for correlated samples. \* significant difference to DXA

A

Regression equation (or set of equations)	BF (method) (%)	Mean difference (DXA - method) (BF %)	SEE (relative to DXA)	p (BF (method) vs. BF DXA)	Difference to DXA based accuracy rank	SEE-based precision rank (relative to DXA)	Sum of ranks for accuracy and precision	Body density (BD) (g/ml) (1 <sup>st</sup> indirect equation)	BF (%) (indirect equation or direct equation)	(2 <sup>nd</sup> )
F 58	25.43	0.058	1.31	0.926	2	2	4	1.1145 - (0.000924 * WC) - (0.000465 * AY)	100*(4.570 eBD - 4.142)	
F 62	25.72	-0.225	1.64	0.659	3	5	8	1.1622 - (0.0654 * log10(BI + TR + SS + IC)) - (0.000574 * AY)	100*(4.570 eBD - 4.142)	
F 66	26.19	-0.698	1.42	0.246	7	3	10	1.1145 - (0.000924 * WC) - (0.000465 * AY)	(495/eBD) - 450	
F 52	24.80	0.696	1.53	0.260	7	4	11	1.06234 - (0.00068 * SS) - (0.00039 * TR) - (0.00025 * TH)	(495/eBD) - 450	
F 67	26.22	-0.726	1.47	0.221	7	4	11		(0.439 * WC) + (0.221 * AY) - 9.4	
F 65	26.12	-0.632	1.82	0.211	6	7	13	1.1599 - (0.0717 * log10(BI + TR + SS + IC))	100*(4.570 eBD - 4.142)	
F 44	24.15	1.345*	1.41	0.041	11	3	14	1.06234 - (0.00068 * SS) - (0.00039 * TR) - (0.00025 * TH)	100*(4.570 eBD - 4.142)	
F 69	26.50	-1.004*	1.77	0.048	8	7	15	1.1622 - (0.0654 * log10(BI + TR + SS + IC)) - (0.000574 * AY)	(495/eBD) - 450	
F 68	26.45	-0.955	1.82	0.056	8	7	15		(30.8 * log10(BI + TR + SS + IC)) + (0.274 * AY) - 31.7	
F 55	25.10	0.394	2.35	0.458	5	13	18	1.1062 - (0.000482 * WC) - (0.00140 * TR) - (0.000453 * AY)	(495/eBD) - 450	
F 60	25.62	-0.131	2.71	0.826	2	16	18	1.1091 - (0.00139 * UAFC) - (0.00126 * TR) - (0.000518 * AY)	(495/eBD) - 450	
F 56	25.10	0.393	2.43	0.459	5	13	18		(0.232 * WC) + (0.657 * TR) + (0.215 * AY) - 5.5	
F 59	25.52	-0.029	2.79	0.961	1	17	18		(0.676 * UAFC) + (0.582 * TR) + (0.246 * AY) - 7.1	
F 49	24.42	1.066	2.17	0.053	9	11	20	1.1062 - (0.000482 * WC) - (0.00140 * TR) - (0.000453 * AY)	100*(4.570 eBD - 4.142)	
F 64	26.10	-0.607	2.56	0.372	6	14	20	1.1299 - (0.00291 * UAFC) - (0.000512 * AY)	100*(4.570 eBD - 4.142)	
F 54	24.91	0.581	2.50	0.330	6	14	20	1.1091 - (0.00139 * UAFC) - (0.00126 * TR) - (0.000518 * AY)	100*(4.570 eBD - 4.142)	
F 50	24.49	1.004	2.32	0.107	8	12	20		(1.2 * BMI) + (0.23 * AY) - (10.8 * 0) - 5.4	
F 72	26.94	-1.445*	1.97	0.006	12	9	21	1.1599 - (0.0717 * (log10(BI + TR + SS + IC)))	(495/eBD) - 450	
F 74	27.11	-1.615*	1.83	0.003	14	7	21	1.1581 - (0.072 * log10(BI + TR + SS + IC))	100*(4.570 eBD - 4.142)	
F 73	27.08	-1.591*	1.86	0.001	14	8	22		(-13.778) + (TR * 0.372) + (SS * 0.17) + (AB * 0.137) + (HC * 0.414) - (UARC * 0.317)	
F 43	24.08	1.412*	2.24	0.027	12	11	23	1.1088 - (0.00254 * BMI) - (0.000551 * AY)	(495/eBD) - 450	
F 75	27.14	-1.646*	2.01	0.001	14	9	23		(-15.471) + (TR * 0.332) + (SS * 0.154) + (AB * 0.119) + (HC * 0.356)	
F 42	24.07	1.422*	2.34	0.025	12	12	24		(1.21 * BMI) + (0.262 * AY) - 6.7	
F 53	24.84	0.652	2.90	0.253	7	18	25	1.1466399 - (0.00093 * (TR + IC + TH)) + (0.0000028 * (TR + IC + TH) * (TR + IC + TH)) - 0.0006171 * HC	(495/eBD) - 450	
F 57	25.10	0.386	3.19	0.538	5	21	26	1.0852 - (0.0008 * IC) - (0.0011 * TH)	100*(4.570 eBD - 4.142)	
F 61	25.65	-0.160	3.47	0.815	3	23	26		(0.503 * AY) + (10.689 * 1) + (3.172 * BMI) - (0.026 * BMI^2) + (0.181 * BMI * 1) - (0.02 * BMI * AY) - (0.005 * BMI^2 * 1) + (0.00021 * BMI^2 * AY) - 44.988	
F 34	23.49	2.005*	2.06	0.003	17	10	27	1.0851 - (0.002 * TR) - (0.000586 * AY)	100*(4.570 eBD - 4.142)	
F 51	24.54	0.956	3.00	0.153	8	19	27		(495/eBD) - 450	
F 39	23.90	1.589*	2.42	0.002	14	13	27	1.1443913 - (0.0006523 * (TR + IC + AB + TH)) + (0.0000014 * (TR + IC + AB + TH) * (TR + IC + AB + TH)) - (0.0006053 * HC)	(495/eBD) - 450	
F 46	24.19	1.304*	2.67	0.018	11	16	27	1.1466399 - (0.00093 * (TR + IC + TH)) + (0.0000028 * (TR + IC + TH) * (TR + IC + TH)) - 0.0006171 * HC	100*(4.570 eBD - 4.142)	
F 63	25.83	-0.343	3.45	0.610	4	23	27	1.0852 - (0.0008 * IC) - (0.0011 * TH)	(495/eBD) - 450	
F 47	24.33	1.159*	2.85	0.046	10	17	27	1.1295 - (0.0007 * IC) - (0.0008 * TH) - (0.0059 * KW)	(495/eBD) - 450	
F 41	24.02	1.470*	2.58	0.013	13	15	28	1.1039 - (0.00148 * BMI) - (0.00122 * TR) - (0.000505 * AY)	(495/eBD) - 450	
F 45	24.17	1.318*	2.79	0.021	11	17	28	1.1470292 - (0.0009376 * (TR + IC + TH)) + (0.000003 * (TR + IC + TH) * (TR + IC + TH)) - (0.0001156 * AY) - (0.0005839 * HC)	(495/eBD) - 450	
F 71	26.91	-1.419*	2.76	0.044	12	17	29	1.1299 - (0.00291 * UAFC) - (0.000512 * AY)	(495/eBD) - 450	
F 48	24.42	1.074	3.10	0.115	9	20	29		(0.944 * TR) + (0.279 * AY) + 4.6	
F 32	23.32	2.169*	2.24	0.000	19	11	30	1.1443913 - (0.0006523 * (TR + IC + AB + TH)) + (0.0000014 * (TR + IC + AB + TH) * (TR + IC + AB + TH)) - (0.0006053 * HC)	100*(4.570 eBD - 4.142)	
F 35	23.50	1.989*	2.36	0.000	17	13	30	1.1454464 - (0.0006558 * (TR + IC + AB + TH)) + (0.0000015 * (TR + IC + AB + TH) * (TR + IC + AB + TH)) - (0.000604 * AY) - (0.0005981 * HC)	(495/eBD) - 450	
F 38	23.72	1.772*	2.63	0.002	15	15	30	1.1295 - (0.0007 * IC) - (0.0008 * TH) - (0.0059 * KW)	100*(4.570 eBD - 4.142)	
F 70	26.88	-1.392*	2.85	0.049	12	18	30		(1.38 * UAFC) + (0.243 * AY) - 16.7	
F 76	28.00	-2.510*	1.98	0.000	22	9	31	1.1581 - (0.072 * log10(BI + TR + SS + IC))	(495/eBD) - 450	
F 33	23.43	2.060*	2.38	0.001	18	13	31	1.1039 - (0.00148 * BMI) - (0.00122 * TR) - (0.000505 * AY)	100*(4.570 eBD - 4.142)	
F 40	23.91	1.585*	2.77	0.020	14	17	31	1.0851 - (0.002 * TR) - (0.000586 * AY)	100*(4.570 eBD - 4.142)	
F 36	23.57	1.919*	2.58	0.001	16	15	31	1.1470292 - (0.0009376 * (TR + IC + TH)) + (0.000003 * (TR + IC + TH) * (TR + IC + TH)) - (0.0001156 * AY) - (0.0005839 * HC)	100*(4.570 eBD - 4.142)	
F 23	22.73	2.761*	1.84	0.000	25	7	32	1.0764 - (0.00081 * IC) - (0.00088 * TR)	(495/eBD) - 450	
F 26	22.95	2.539*	2.17	0.000	22	11	33	1.1454464 - (0.0006558 * (TR + IC + AB + TH)) + (0.0000015 * (TR + IC + AB + TH) * (TR + IC + AB + TH)) - (0.000604 * AY) - (0.0005981 * HC)	100*(4.570 eBD - 4.142)	
F 31	23.16	2.328*	2.64	0.000	20	15	35	1.12569 - (0.001835 * TR) - (0.002779 * (0.3937 * HC)) + (0.005419 * (0.3937 * UAFC)) - (0.0007167 * SS)	(495/eBD) - 450	
F 14	22.24	3.251*	1.70	0.000	30	6	36	1.0764 - (0.00081 * IC) - (0.00088 * TR)	100*(4.570 eBD - 4.142)	
F 28	23.06	2.426*	2.64	0.000	21	15	36	1.18666 - (0.07032 * log10(TR + SS + SSP + TH)) - (0.000928 * HC) + (0.00115 * CC) + (0.00529 * EW)	(495/eBD) - 450	
F 24	22.79	2.705*	2.34	0.000	24	12	36	1.0836 - (0.0007 * IC) - (0.0007 * TH) + (0.0048 * WRC) - (0.0088 * KW)	(495/eBD) - 450	
F 37	23.61	1.885*	3.07	0.004	16	20	36	1.0994921 - (0.000929 * (TR + IC + TH)) + (0.0000023 * (TR + IC + TH) * (TR + IC + TH)) - (0.0001392 * AY)	(495/eBD) - 450	
F 29	23.12	2.375*	2.64	0.000	21	15	36		(0.730 * BMI) + (0.548 * TR) + (0.270 * AY) - 5.9	
F 25	22.88	2.611*	2.52	0.000	23	14	37	1.096095 - (0.0006952 * (TR + IC + AB + TH)) + (0.0000011 * (TR + IC + AB + TH) * (TR + IC + AB + TH)) - (0.0000714 * AY)	(495/eBD) - 450	
F 27	23.05	2.442*	2.83	0.000	21	17	38	1.0994921 - (0.000929 * (TR + IC + TH)) + (0.0000023 * (TR + IC + TH) * (TR + IC + TH)) - (0.0001392 * AY)	100*(4.570 eBD - 4.142)	
F 22	22.64	2.851*	2.44	0.000	26	13	39	1.12569 - (0.001835 * TR) - (0.002779 * (0.3937 * HC)) + (0.005419 * (0.3937 * UAFC)) - (0.0007167 * SS)	100*(4.570 eBD - 4.142)	
F 21	22.55	2.942*	2.44	0.000	26	13	39	1.18666 - (0.07032 * log10(TR + SS + SSP + TH)) - (0.000928 * HC) + (0.00115 * CC) + (0.00529 * EW)	100*(4.570 eBD - 4.142)	
F 16	22.29	3.199*	2.16	0.000	29	11	40	1.0836 - (0.0007 * IC) - (0.0007 * TH) + (0.0048 * WRC) - (0.0088 * KW)	100*(4.570 eBD - 4.142)	
F 19	22.38	3.113*	2.33	0.000	28	12	40	1.096095 - (0.0006952 * (TR + IC + AB + TH)) + (0.0000011 * (TR + IC + AB + TH) * (TR + IC + AB + TH)) - (0.0000714 * AY)	100*(4.570 eBD - 4.142)	
F 18	22.36	3.131*	2.47	0.000	28	14	42	1.20953 - (0.08294 * log10(TR + SS + AB + TH + SSP + CA))	(495/eBD) - 450	
F 20	22.48	3.008*	2.64	0.000	27	15	42	1.2032 - (0.08169 * log10(TR + SSP + AB + TH + CA))	(495/eBD) - 450	
F 30	23.15	2.485*	3.44	0.001	20	22	42		(0.61 * (CA + TR)) + 5.1	
F 1	8.06	17.436*	0.67	0.000	41	1	42		((0.14 * (AB + TR + SS)) * (BH * 100)^(3/2) * 0.0001) + 3.2 / BM * 100	
F 15	22.27	3.221*	2.57	0.000	29	15	44		(1.33 * (TR + SS)) * (0.013 * (TR + SS)) * (TR + SS) - 2.5	
F 77	28.51	-3.022*	2.85	0.000	27	17	44		((0.11 * (AB + TR + SS)) * (BH * 100) * (BH * 100) * 0.0001) + 3.1 / BM * 100	
F 12	21.90	3.593*	2.28	0.000	33	12	45	1.20953 - (0.08294 * log10(TR + SS + AB + TH + SSP + CA))	100*(4.570 eBD - 4.142)	
F 13	22.01	3.480*	2.44	0.000	32	13	45	1.2032 - (0.08169 * log10(TR + SSP + AB + TH + CA))	100*(4.570 eBD - 4.142)	
F 78	28.88	-3.392*	2.72	0.000	31	16	47		22.18945 * (AY * 0.06368) + (BMI * 0.60404) - ((BH * 100) * 0.1452) + ((TR + SS + IC + TH) * 0.30919) - ((TR + SS + IC + TH) * (TR + SS + IC + TH) * 0.00099562)	
F 4	19.66	5.833*	2.10	0.000	39	10	49	1.09246 - (0.00049 * SS) - (0.00075 * IC) + (0.00710 * EW) - (0.00121 * TC)	100*(4.570 eBD - 4.142)	
F 6	19.93	5.557*	2.27	0.000	37	12	49	1.09246 - (0.00049 * SS) - (0.00075 * IC) + (0.00710 * EW) - (0.00121 * TC)	(495/eBD) - 450	
F 2	15.56	9.932*	1.98	0.000	40	9	49		(0.24 * BM) + 0.21 * (AB + TR + SS) - 7.3	
F 9	21.07	4.422*	2.80	0.000	35	17	52	1.2035 - (0.08715 * log10(TR + SS + SSP + TH))	100*(4.570 eBD - 4.142)	
F 11	21.46	4.029*	3.04	0.000	34	19	53	1.2035 - (0.08715 * log10(TR + SS + SSP + TH))	(495/eBD) - 450	
F 17	22.31	3.184*	4.28	0.001	29	25	54		(4.35 * BMI) - (0.05 * BMI * BMI) - 46.24	
F 8	21.06	4.428*	3.23	0.000	35	21	56	1.19461 - (0.08642 * log10(TR + SSP + TH))	100*(4.570 eBD - 4.142)	
F 10	21.46	4.035*	3.50	0.000	34	23	57	1.19461 - (0.08642 * log10(TR + SSP + TH))	(495/eBD) - 450	
F 7	20.58	4.908*	4.00	0.000	36	24	60		((0.0581 * AY) + (0.507 * BM) - (0.256 * BH * 100) + (0.165 * HC) + 8.68) / BM * 100	
F 5	19.77	5.723*	4.01	0.000	38	24	62		((0.631 * BM) + (0.0629 * AY) - (0.273 * BH * 100) + 19.6) / BM * 100	
F 3	19.65	5.841*	4.36	0.000	39	26	65		(0.632 - (0.632 * (15 / BMI)) + (0.00135 * AY)) * 100	

B

Regression equation (or set of equations)	BF (method) (%)	Mean difference (DXA - method) (BF: %)	SEE (relative to DXA)	p (BF (method) vs. BF DXA)	Difference to DXA based accuracy rank	SEE-based precision rank (relative to DXA)	Sum of ranks for accuracy and precision	Body density (BD) (g/ml) (1 <sup>st</sup> indirect equation)	BF (%) (2 <sup>nd</sup> indirect equation or direct equation)
M 35	13.83	0.101	2.03	0.891	2	11	13		$((0.158 * BM + 0.383 * WC - 0.118 * BH * 100 - 10.2) / BM) * 100$
M 31	13.28	0.652	1.75	0.178	7	8	15	$1.1554 - (0.000761 * WC) - (0.00170 * TR) - (0.000532 * AY)$	$100 * (4.570 / BD - 4.142)$
M 38	14.18	-0.245	2.25	0.606	3	14	17		$(1.21 * (TR + SS)) - (0.008 * (TR + SS)) + (TR + SS) - 5.5$
M 26	12.85	1.083*	1.62	<b>0.005</b>	11	7	18		$(0.735 * (TR + CA)) + 1$
M 25	12.76	1.177*	1.56	<b>0.006</b>	12	7	19		$((((0.00285 * (TR + SS) / 2) - 0.0114) * 0.5 - 0.061 * BM) + (1.1 * (BH * BH * BH) + (0.234 * AY - 6.4) / BM) * 100$
M 29	13.10	0.834	1.99	0.102	8	11	19		$(0.353 * WC) + (0.756 * TR) + (0.235 * AY) - 26.4$
M 28	13.03	0.906	1.89	0.070	9	10	19	$1.1554 - (0.000761 * WC) - (0.0017 * TR) - (0.000532 * AY)$	$(495 / BD) - 450$
M 44	14.89	-0.958*	1.83	<b>0.025</b>	10	9	19	$1.1862 - (0.0684 * \log_{10}(BI + TR + SS + IC)) - (0.000601 * AY)$	$100 * (4.570 / BD - 4.142)$
M 42	14.77	-0.837	1.99	0.059	8	11	19	$1.1862 - (0.0684 * \log_{10}(BI + TR + SS + IC)) - (0.000601 * AY)$	$(495 / BD) - 450$
M 41	14.70	-0.767	2.13	0.245	8	12	20		$((-0.103 * BM + 0.345 * WC + 0.485 * HC - 55.2) / BM) * 100$
M 34	13.74	0.189	2.68	0.739	3	17	20	$1.103 - (0.00168 * SS) - (0.00127 * AB)$	$100 * (4.570 / BD - 4.142)$
M 37	13.93	0.001	2.96	0.999	1	19	20		$((-0.470 * (0.397 * WC) + (6.568 * (\log_{10}(TR) + \log_{10}(SS) + \log_{10}(AB)))) / BM) * 100$
M 43	14.80	-0.867	2.08	0.059	9	12	21		$(30.9 * \log_{10}(BI + TR + SS + IC)) + (0.271 * AY) - 39.9$
M 32	13.41	0.520	2.52	0.334	6	16	22	$1.02415 - (0.00169 * SS) + (0.00444 * BH * 10) - (0.0013 * AB)$	$100 * (4.570 / BD - 4.142)$
M 18	11.31	2.627*	1.22	<b>0.000</b>	19	3	22	$1.09665 - (0.00103 * TR) - (0.00056 * SS) - (0.00054 * AB)$	$100 * (4.570 / BD - 4.142)$
M 45	14.93	-0.993	2.05	0.188	10	12	22		$(0.567 * WC) + (0.101 * AY) - 31.8$
M 50	15.23	-1.300	1.82	0.080	13	9	22	$1.1674 - (0.00125 * WC) - (0.000231 * AY)$	$100 * (4.570 / BD - 4.142)$
M 27	12.92	1.009*	2.09	<b>0.046</b>	10	12	22	$1.1414 - (0.0016 * BMI) - (0.00213 * TR) - (0.000747 * AY)$	$100 * (4.570 / BD - 4.142)$
M 36	13.85	0.081	3.14	0.920	2	20	22		$((1.003 * WC) - (66.475 * (WC / HC)) - 21.364 * 0.92) / BM) * 100$
M 33	13.53	0.405	2.90	0.510	5	18	23	$1.103 - (0.00168 * SS) - (0.00127 * AB)$	$(495 / BD) - 450$
M 48	15.14	-1.208	1.97	0.109	12	11	23	$1.1674 - (0.00125 * WC) - (0.000231 * AY)$	$(495 / BD) - 450$
M 40	14.36	-0.424	2.87	0.507	5	18	23	$1.1613 - (0.00165 * UAFC) - (0.00238 * TR) - (0.000882 * AY)$	$100 * (4.570 / BD - 4.142)$
M 52	15.75	-1.815*	1.66	<b>0.000</b>	16	8	24	$1.1631 - 0.0632 * (\log_{10}(BI + TR + SS + IC))$	$100 * (4.570 / BD - 4.142)$
M 39	14.19	-0.258	3.11	0.702	4	20	24	$1.1613 - (0.00165 * UAFC) - (0.00238 * TR) - (0.000882 * AY)$	$(495 / BD) - 450$
M 51	15.70	-1.765*	1.80	<b>0.000</b>	16	9	25	$1.1631 - 0.0632 * (\log_{10}(BI + TR + SS + IC))$	$(495 / BD) - 450$
M 30	13.17	0.764	2.73	0.194	8	17	25	$1.02415 - (0.00169 * SS) + (0.00444 * BH * 10) - (0.0013 * AB)$	$(495 / BD) - 450$
M 55	16.09	-2.162*	1.74	<b>0.000</b>	17	8	25	$-0.0662 * \log_{10}(BI + TR + SS + IC) + 1.167$	$100 * (4.570 / BD - 4.142)$
M 17	10.89	3.046*	1.32	<b>0.000</b>	21	4	25	$1.09665 - (0.00103 * TR) - (0.00056 * SS) - (0.00054 * AB)$	$(495 / BD) - 450$
M 21	12.10	1.831*	1.83	<b>0.000</b>	16	9	25	$1.1181 - (0.00289 * TR) - (0.000953 * AY)$	$100 * (4.570 / BD - 4.142)$
M 47	15.11	-1.177	2.19	0.116	12	13	25	$1.1419 - (0.0029 * BMI) - (0.000527 * AY)$	$100 * (4.570 / BD - 4.142)$
M 46	15.01	-1.074	2.37	0.160	11	15	26	$1.1419 - (0.0029 * BMI) - (0.000527 * AY)$	$(495 / BD) - 450$
M 54	16.07	-2.141*	1.88	<b>0.000</b>	17	10	27	$-0.0662 * \log_{10}(BI + TR + SS + IC) + 1.167$	$(495 / BD) - 450$
M 24	12.64	1.293*	2.26	0.017	13	14	27	$1.1414 - (0.0016 * BMI) - (0.00213 * TR) - (0.000747 * AY)$	$(495 / BD) - 450$
M 56	16.60	-2.666*	1.67	<b>0.000</b>	20	8	28	$1.161 - 0.0632 * (\log_{10}(BI + TR + SS + IC))$	$100 * (4.570 / BD - 4.142)$
M 20	11.75	2.183*	1.98	<b>0.000</b>	17	11	28	$1.1181 - (0.00289 * TR) - (0.000953 * AY)$	$(495 / BD) - 450$
M 49	15.16	-1.232	2.49	0.116	12	16	28		$(1.33 * BMI) + (0.236 * AY) - 20.2$
M 57	16.62	-2.687*	1.80	<b>0.000</b>	20	9	29	$1.161 - 0.0632 * (\log_{10}(BI + TR + SS + IC))$	$(495 / BD) - 450$
M 23	12.53	1.398*	2.38	0.013	14	15	29		$(0.742 * BMI) + (0.95 * TR) + (0.335 * AY) - 20$
M 19	11.67	2.267*	2.08	<b>0.000</b>	18	12	30		$(1.31 * TR) + (0.43 * AY) - 9.16$
M 53	16.07	-2.137*	2.26	0.008	17	14	31		$(1.20 * BMI) + (0.23 * AY) - (10.8 * 1) - 5.4$
M 22	12.33	1.603*	3.06	0.022	15	20	35		$(0.757 * UAFC) + (1.07 * TR) + (0.398 * AY) - 29$
M 7	8.57	5.359*	0.67	<b>0.000</b>	34	2	36	$1.0982 - 0.000815 * (TR + SS + AB) + 0.0000084 * (TR + SS + AB) * (TR + SS + AB)$	$100 * (4.570 / BD - 4.142)$
M 63	18.76	-4.829*	1.48	<b>0.000</b>	30	6	36		$20.94878 + (AY * 0.1166) - (BH * 100 * 0.11666) + ((TR + SS + IC + TH) * 0.42696) - ((TR + SS + IC + TH) * (TR + SS + IC + TH) * 0.00159)$
M 6	7.93	6.004*	0.72	<b>0.000</b>	35	2	37	$1.0982 - 0.000815 * (TR + SS + AB) + 0.0000084 * (TR + SS + AB) * (TR + SS + AB)$	$(495 / BD) - 450$
M 12	9.34	4.590*	1.77	<b>0.000</b>	28	9	37	$1.0996 - 0.001398 * AB$	$100 * (4.570 / BD - 4.142)$
M 16	10.84	3.095*	2.46	<b>0.000</b>	22	16	38	$1.1043 - (0.001327 * TH) - (0.00131 * SS)$	$100 * (4.570 / BD - 4.142)$
M 4	7.40	6.535*	1.24	<b>0.000</b>	37	3	40	$1.1012 - 0.00177 * SS$	$100 * (4.570 / BD - 4.142)$
M 5	7.90	6.031*	1.40	<b>0.000</b>	35	5	40	$1.1034 - 0.002313 * TR$	$100 * (4.570 / BD - 4.142)$
M 1	5.86	8.073*	0.56	<b>0.000</b>	40	1	41		$((0.14 * (AB + TR + SS)) * (BH * 100) * (3/2) * 0.0001) + 3.2) / BM) * 100$
M 15	10.38	3.553*	2.66	<b>0.000</b>	24	17	41	$1.1043 - (0.001327 * TH) - (0.00131 * SS)$	$(495 / BD) - 450$
M 9	8.76	5.172*	1.91	<b>0.000</b>	33	10	43	$1.0996 - 0.001398 * AB$	$(495 / BD) - 450$
M 2	6.65	7.278*	1.34	<b>0.000</b>	39	4	43	$1.1012 - 0.00177 * SS$	$(495 / BD) - 450$
M 13	9.53	4.399*	2.74	<b>0.000</b>	27	17	44	$0.162 + (0.8 * (((100 * BH) * 0.242) / ((1000 * BM) * 0.1)))$	$100 * (4.570 / BD - 4.142)$
M 60	17.65	-3.716*	2.97	<b>0.000</b>	25	19	44		$(0.24 * BMI) + 0.21 * (AB + TR + SS) - 7.3$
M 3	7.20	6.733*	1.51	<b>0.000</b>	38	6	44	$1.1034 - 0.002313 * TR$	$(495 / BD) - 450$
M 59	17.11	-3.178*	3.28	<b>0.001</b>	23	22	45		$0.503 * AY + (10.689 * 0) + (3.172 * BMI) - (0.026 * BMI^2) + (0.181 * BMI * 0) - (0.02 * BMI * AY) - (0.005 * BMI^2 * 0) + (0.00021 * BMI^2 * AY) - 44.988$
M 58	17.07	-3.142*	3.54	<b>0.002</b>	22	23	45		$(3.76 * BMI) - (0.04 * BMI * BMI) - 47.80$
M 65	20.22	-6.291*	1.87	<b>0.000</b>	36	10	46		$((0.11 * (AB + TR + SS)) * (BH * 100) * (BH * 100) * 0.0001) + 3.1) / BM) * 100$
M 11	9.29	4.644*	2.96	<b>0.000</b>	28	19	47	$0.75 + (0.22 * (((100 * BH) * 0.725) / ((1000 * BM) * 0.3)))$	$100 * (4.570 / BD - 4.142)$
M 14	9.86	4.072*	3.52	<b>0.000</b>	26	23	49		$(0.481 - (0.481 * (19.8 / BMI))) + (0.00176 * AY) * 100$
M 10	8.97	4.965*	2.97	<b>0.000</b>	31	19	50	$0.162 + (0.8 * (((100 * BH) * 0.242) / ((1000 * BM) * 0.1)))$	$(495 / BD) - 450$
M 61	18.50	-4.567*	3.93	<b>0.000</b>	28	24	52	$1.1828 - (0.00333 * UAFC) - (0.000745 * AY)$	$100 * (4.570 / BD - 4.142)$
M 8	8.70	5.231*	3.21	<b>0.000</b>	33	21	54	$0.75 + (0.22 * (((100 * BH) * 0.725) / ((1000 * BM) * 0.3)))$	$(495 / BD) - 450$
M 62	18.68	-4.746*	4.26	<b>0.000</b>	29	25	54	$1.1828 - (0.00333 * UAFC) - (0.000745 * AY)$	$(495 / BD) - 450$
M 64	18.98	-5.051*	4.36	<b>0.000</b>	32	26	58		$(1.52 * UAFC) + (0.336 * AY) - 38.7$
M 66	27.66	-13.730*	7.57	<b>0.000</b>	41	27	68	$1.1070 - (0.003845 * TH) - (0.001493 * IC)$	$100 * (4.570 / BD - 4.142)$
M 67	28.60	-14.671*	8.20	<b>0.000</b>	42	28	70	$1.1070 - (0.003845 * TH) - (0.001493 * IC)$	$(495 / BD) - 450$

It has to be noted that upper arm circumference was sometimes [1, 2] measured with elbow flexed at 90° (but with biceps not activated maximally as with "flexed upper arm circumference" according to Lohman et al. [3]), although the existing standardised procedures recommend the same measurement be performed with arm relaxed and extended [3, 4]. Also, to enable comparison between different regression equations (or sets of equations), a constant fat tissue density (0.92 g/ml) (following the protocol of Al-Gindan et al. [5]) had to be used in some [6] equations, to transform adipose tissue volume into body fat mass, although fat tissue density has been demonstrated to vary to a certain extent [7]; such procedure will inevitably decrease the final accuracy of BF determination.

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